



CCEFP Project 16HS3: Controlled Stirling Power Unit

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Outline

- Project Overview
- Methods of Control
 - Controlled Displacer Motion
 - Controlled Inter-Unit Mass Flow
- Potential Applications
- Next Steps
- Conclusion



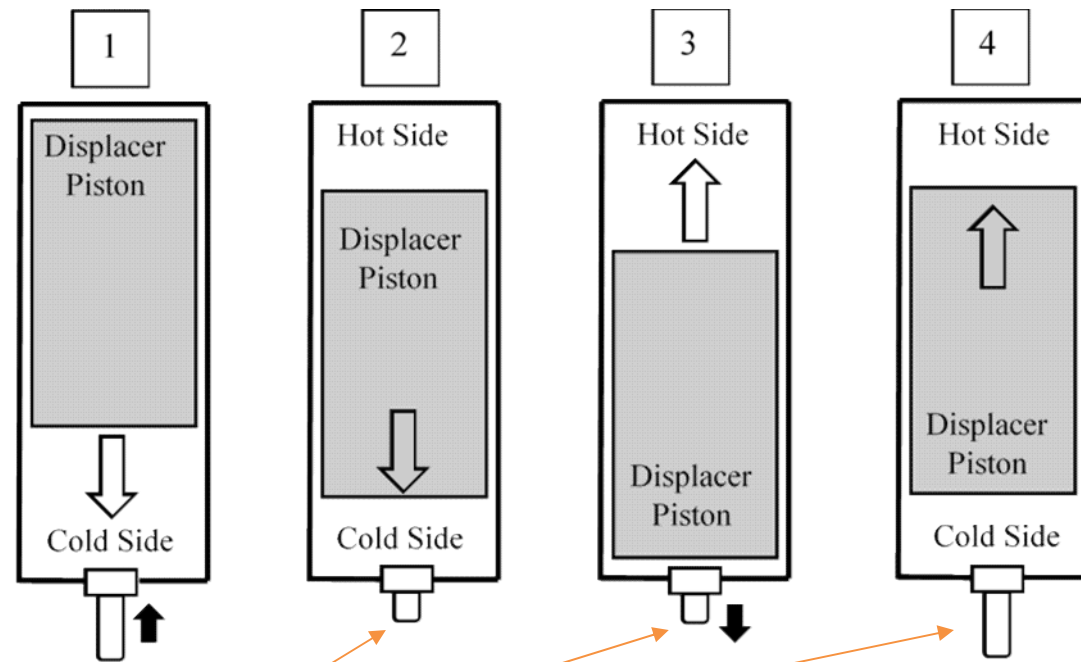
Controlled Stirling Power Unit



- Capable of using heat from many different sources, including waste heat.
- Output power can be hydraulic, pneumatic, mechanical, or electric
- Virtually noiseless operation
- Low maintenance
- Efficient (Stirling cycle approaches Carnot efficiency at high temperatures and pressures)
- Thermodynamics can be controlled

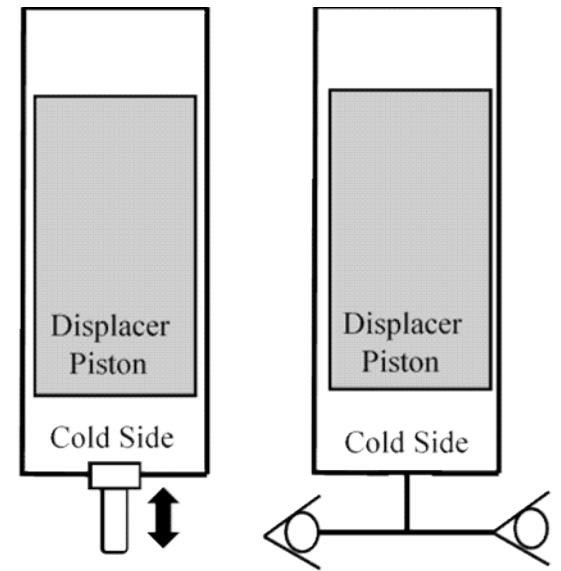


Stirling Engine Cycle



Power Piston

Thermocompressor Arrangement





The Beale Number

$$P \propto V_0 \times f \times p$$

Controlled Displacer Piston

- Decoupled from power piston
- Multiple motion profiles

P = Output power (watts)

p = Median operating pressure (Pa)

f = Power piston frequency (Hz)

V_0 = Volume displaced by power piston (m³)



Model and Verification

$$\dot{U} = \dot{H} + \dot{Q} - \dot{W}$$

$$\dot{U} = \dot{m}(c_v)T + m(c_v)\dot{T} = \frac{1}{\gamma - 1}(\dot{P}V + P\dot{V})$$

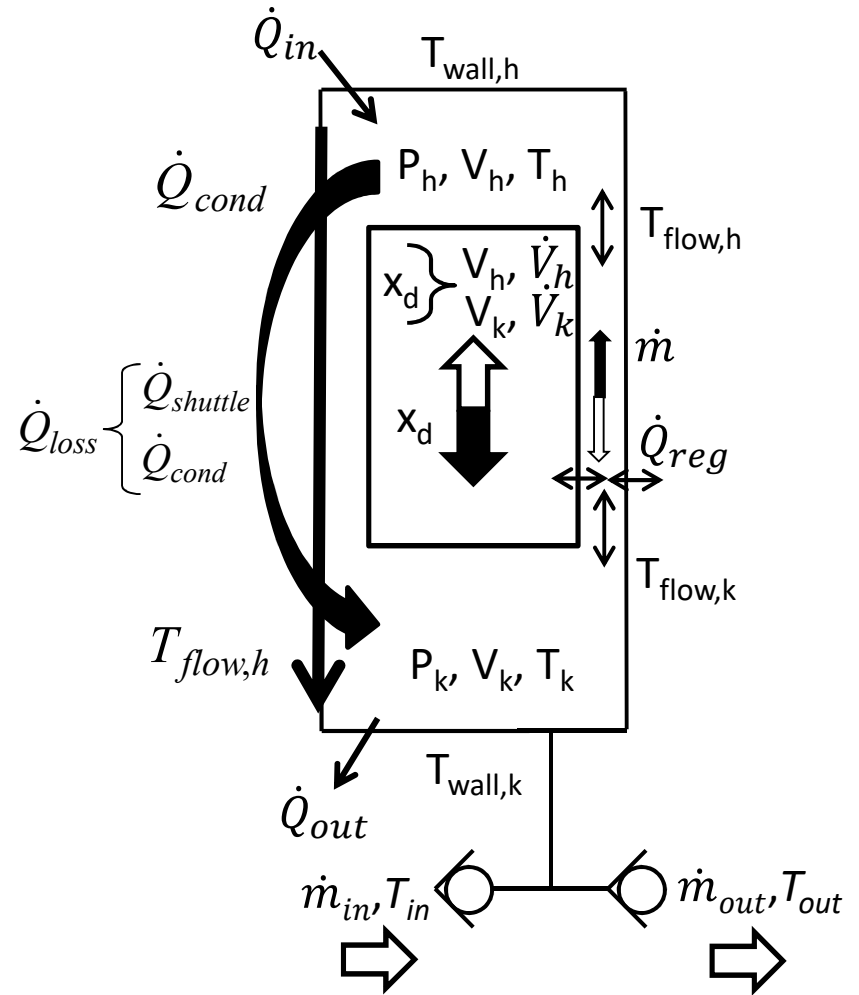
$$\dot{H} = \sum_k \dot{m}_k (c_p)_k (T)_k$$

$$\dot{W} = P\dot{V}$$

$$R = c_p - c_v$$

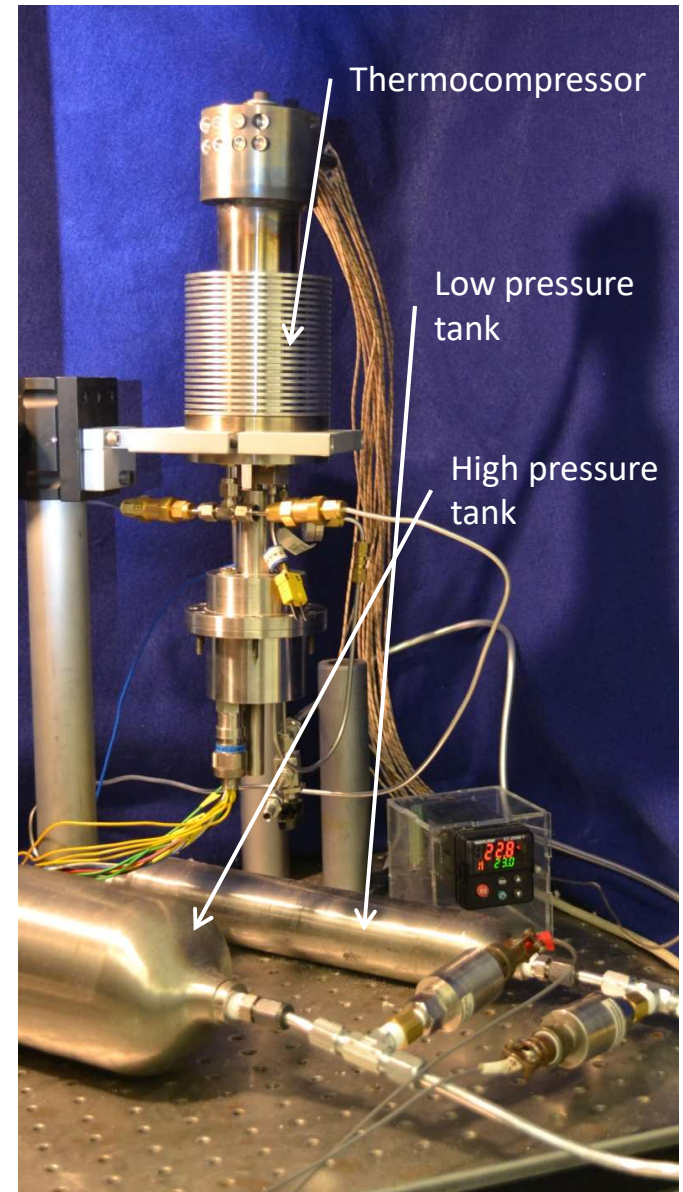
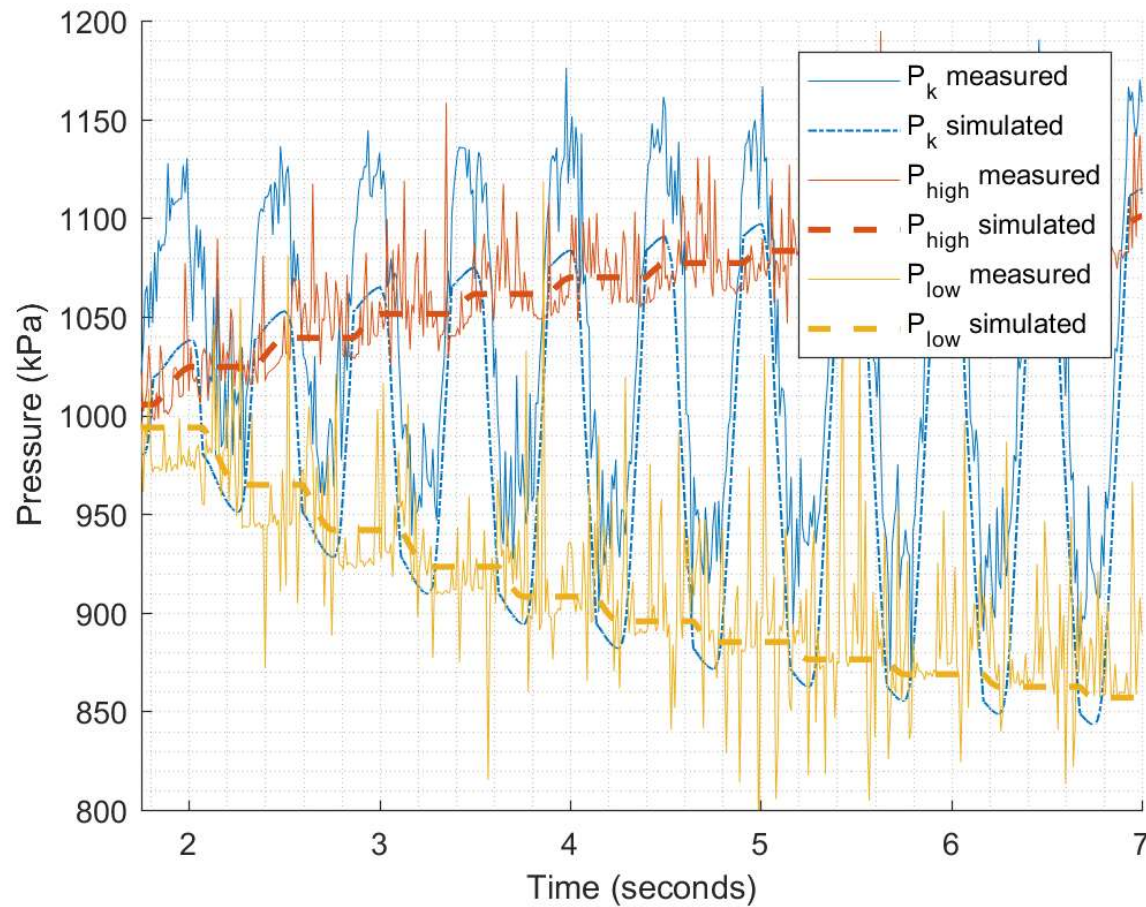
$$\gamma = \frac{c_p}{c_v}$$

$$\dot{P} = \frac{\sum_k \dot{m}_k T_k (R\gamma) + \dot{Q}(\gamma - 1) - P\dot{V}\gamma}{V}$$





Controlled Displacer





The Beale Number

$$P \propto V_0 \times f \times p$$

Controlled Displacer Piston

- Decoupled from power piston
- Multiple motion profiles

Controlled Mass Flow

- Pressure controlled from mass injected at strategic stages

P = Output power (watts)

p = Median operating pressure (Pa)

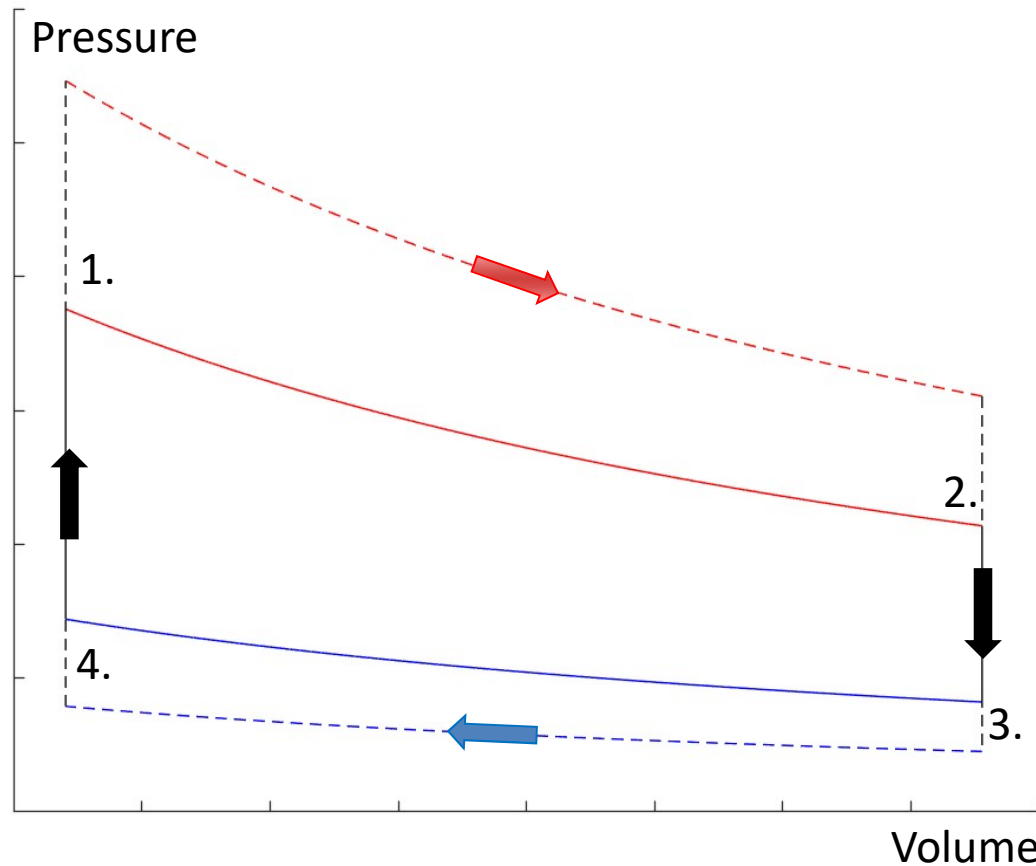
f = Power piston frequency (Hz)

V_0 = Volume displaced by power piston (m³)



Controlled Inter-Unit Mass Flow

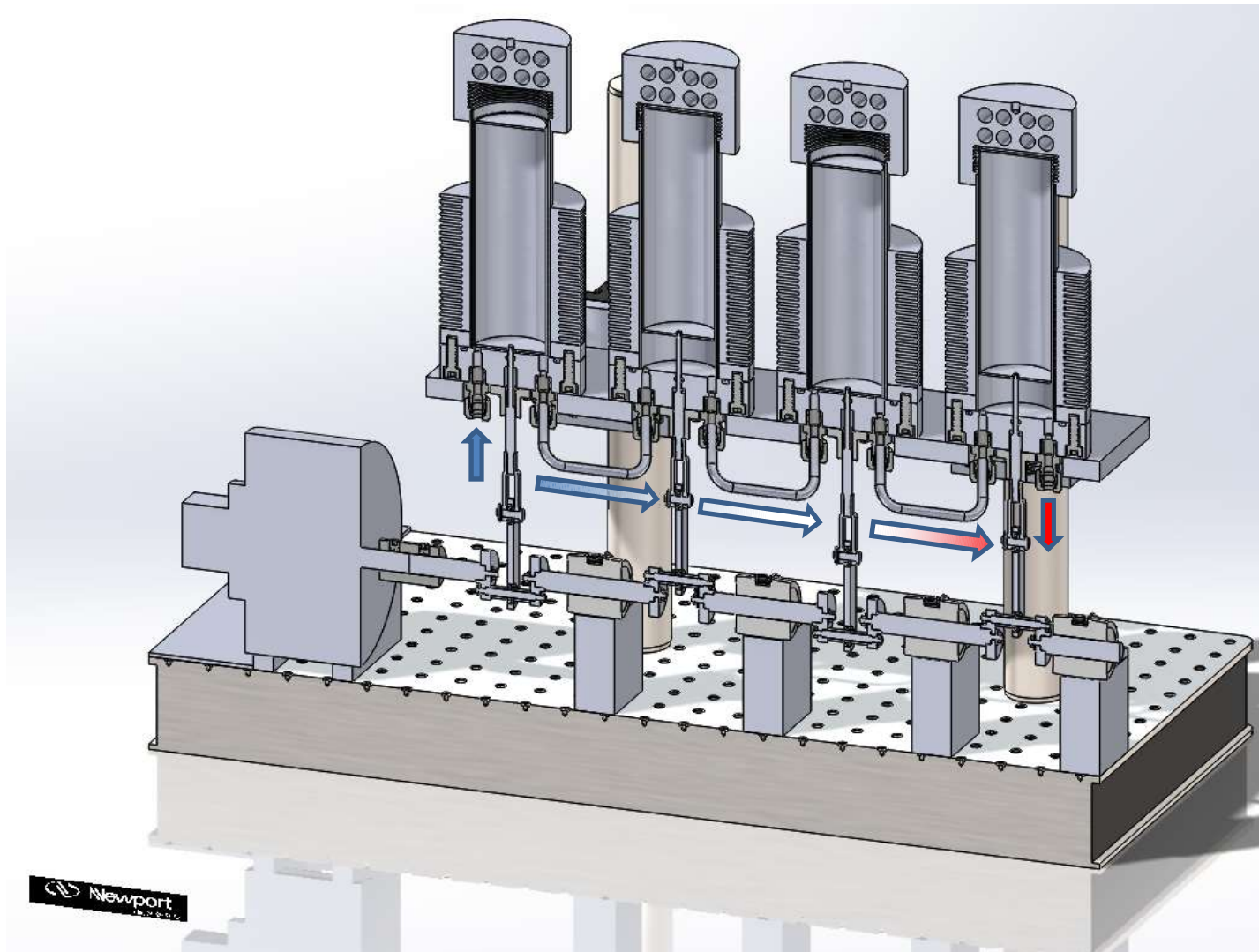
Ideal Stirling Cycle



1. Isothermal Process (Work Out)
2. Isochoric Process
3. Isothermal Process (Work In)
4. Isochoric Process

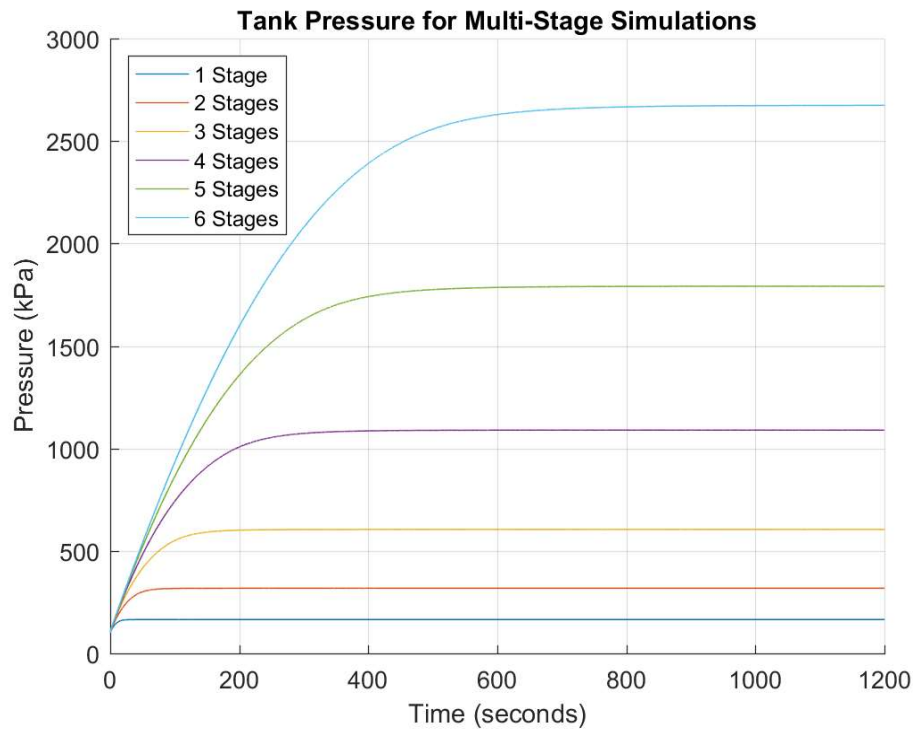


Inter-Unit Mass Flow Simulation





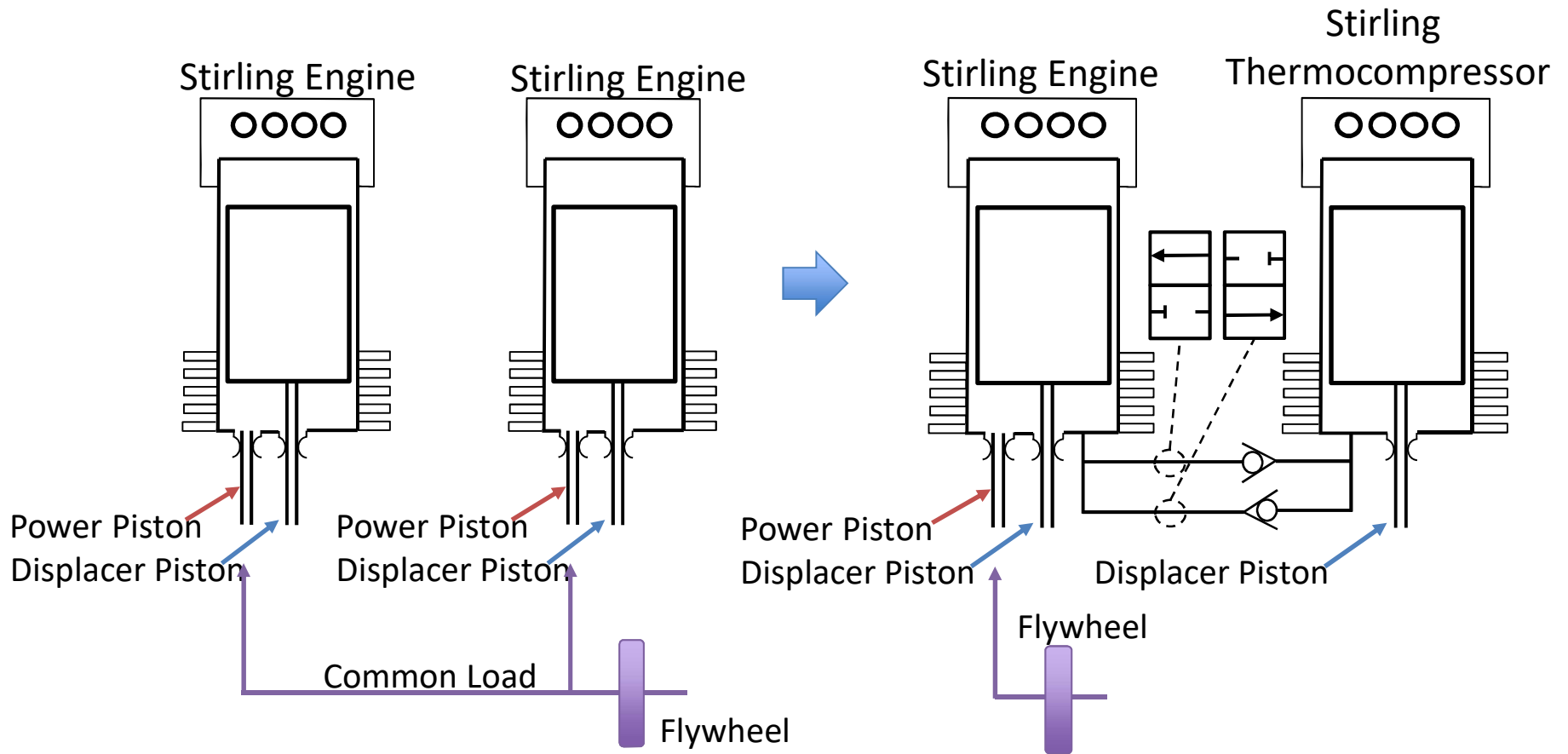
Inter-Unit Mass Flow Simulation



Number of Stages	Steady State Pressure		Adjusted Steady-State Pressure	
	kPa	psia	kPa	psia
1	165.2	24.0	145.6	21.1
2	317.8	46.1	253.2	36.7
3	604.8	87.7	453.9	65.8
4	1,089.6	158.0	789.8	114.5
5	1,791.5	259.8	1,266.9	183.7
6	2,674.0	387.9	1,855.3	269.1

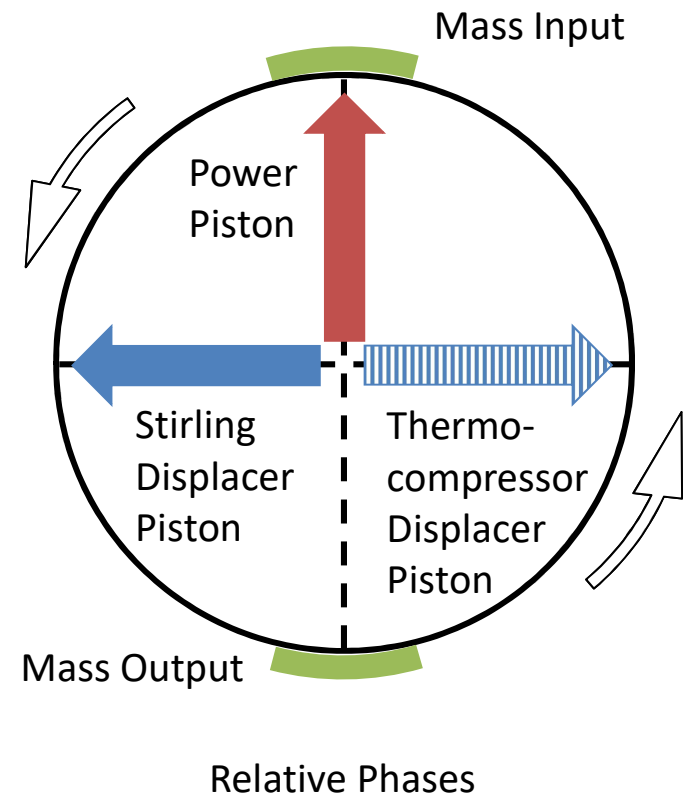
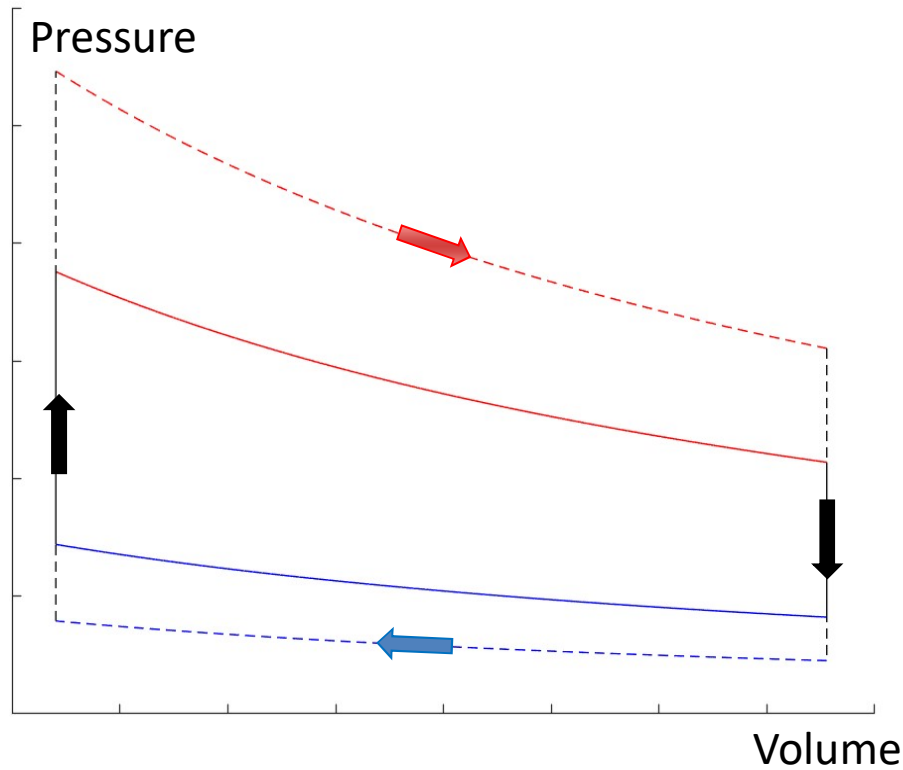


Conceptual Architecture



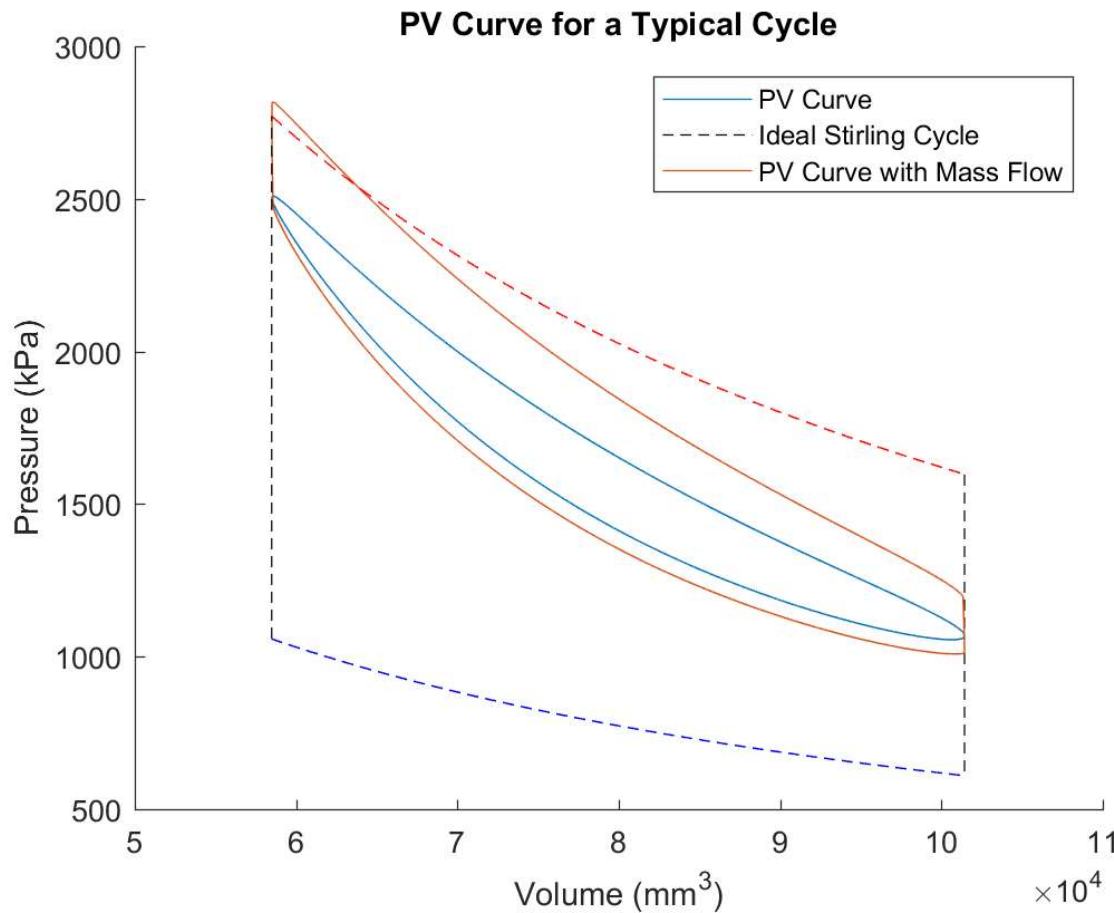


Conceptual Architecture





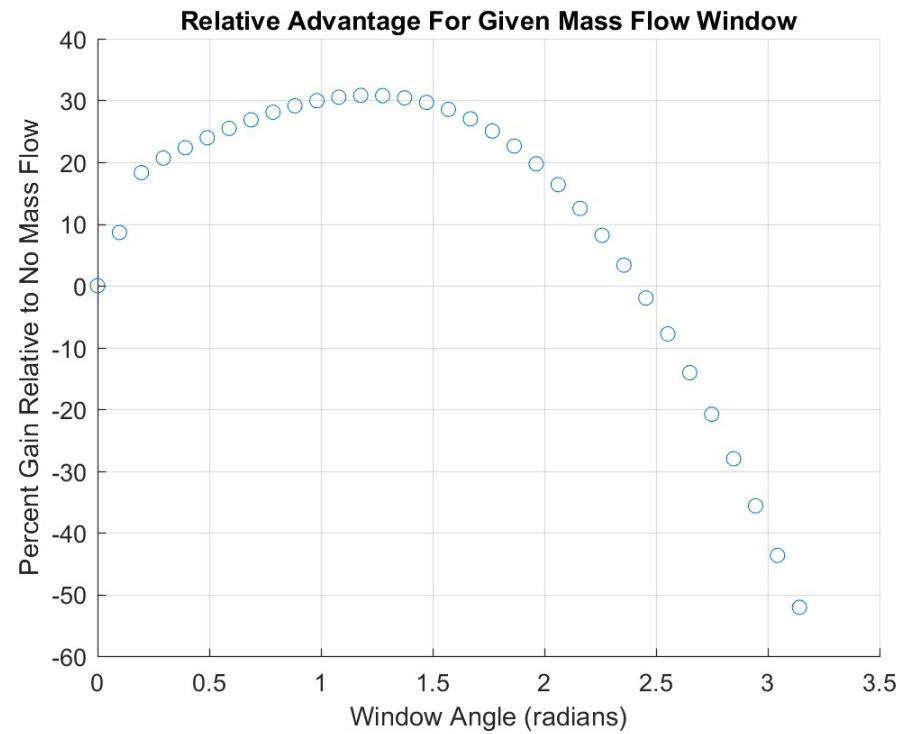
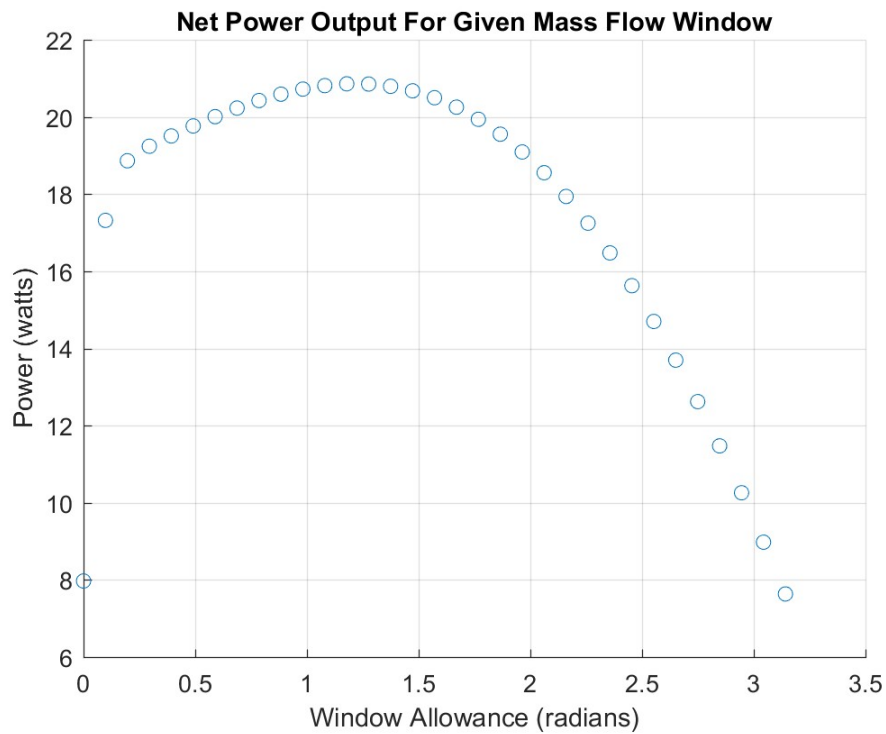
Simulation Results



Mass Flow Window	$\pi/16$ radians
Modelled Power Piston Displacement	42.94 cm ³
Frequency	1 Hz
Median Operating Pressure	16.57 bar
Net Power Output (no mass flow)	7.97 watts
Net Power Output (mass flow)	18.86 watts
Relative Power Gain	2.92 watts (18.34%)



Controlled Mass Flow Window Range





Potential Applications

Increased Power Density in Multi-Engine Systems

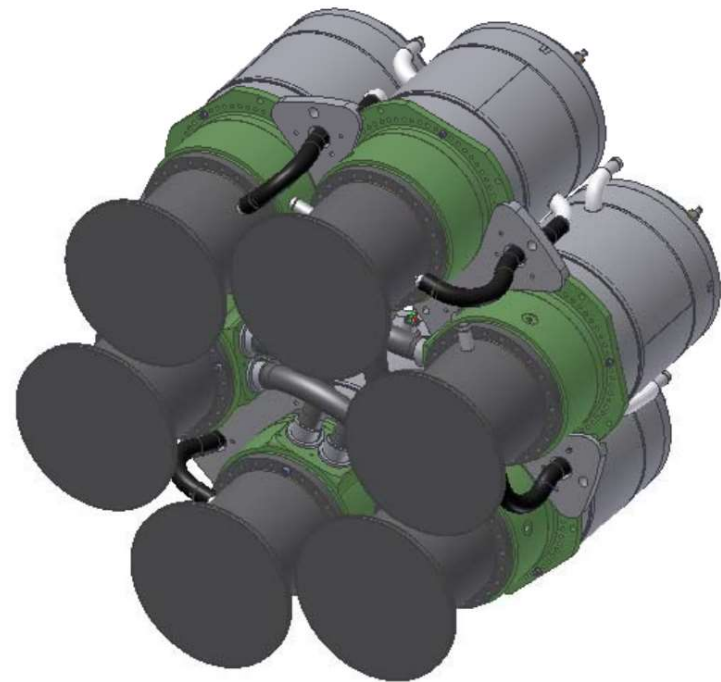


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Potential Applications

Increased Power Density in Multi-Engine Systems

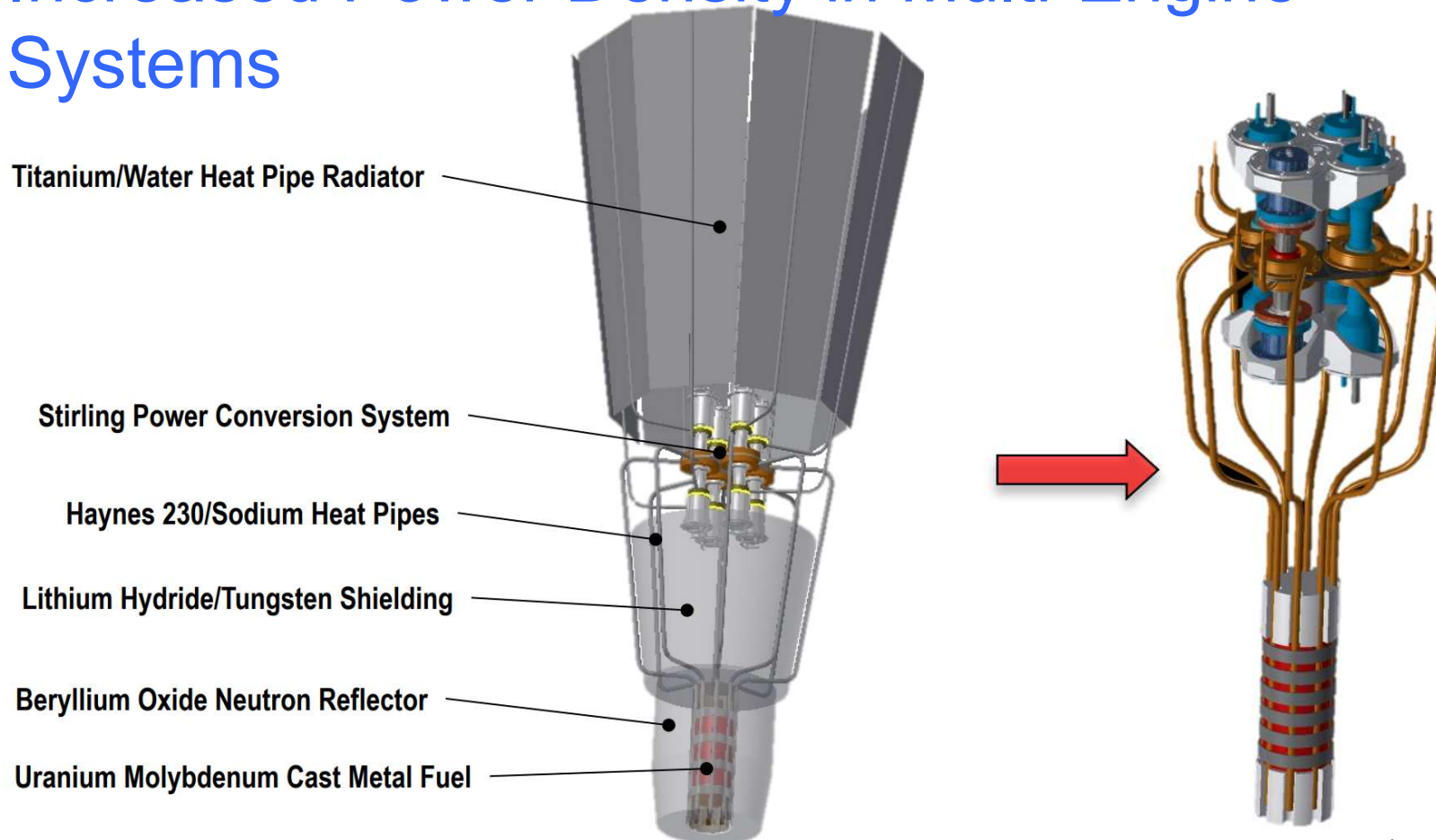
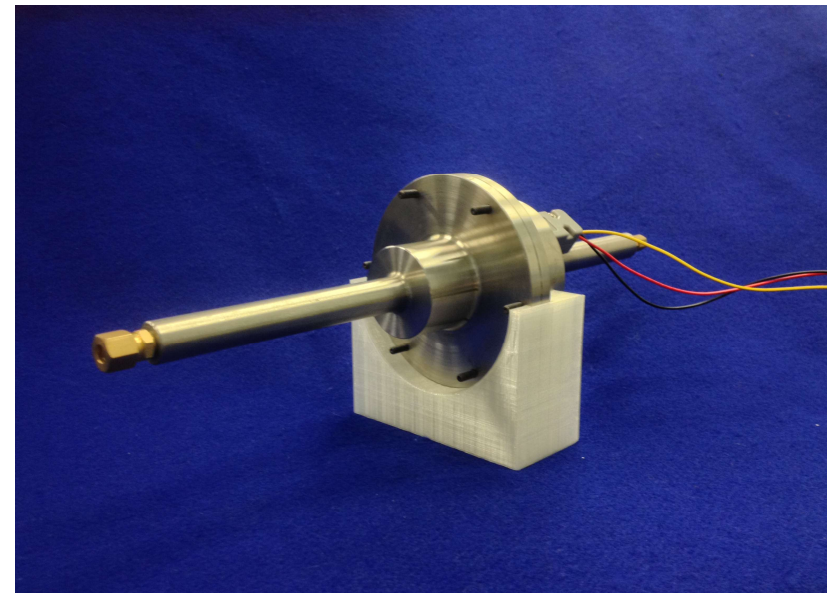


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Next Steps

- Validate Controlled Mass Flow Simulation Results with Experimental Data
 - Install Linear Alternator on Current Stirling Thermocompressor to make a Traditional Stirling Engine
 - Emulate Thermocompressor Pressure Oscillations Using Reservoirs Held at High/Low Temperatures, Pressures
 - Regulate Mass Flow using Control Valves
- Experimentally Validate Full Control of Stirling Engine



Linear Alternator



Conclusions

- A control strategy for increasing power output from Stirling devices using controlled mass flow from accompanying Stirling thermocompressors was introduced and simulated.
- Simulation results corroborate that power output can be greater using an engine-thermocompressor arrangement than with an equivalent pair of Stirling engines. Experimental validation is forthcoming.
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 - eric.j.barth@vanderbilt.edu



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